



FE-Analysis by the additional module ROHR2fesu

Program System ROHR2

SIGMA Ingenieurgesellschaft mbH





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1 ROHR2fesu Overview

ROHR2fesu is an additional module in the program system ROHR2 for detailed analysis of local segments in pipes and vessels.

ROHR2fesu offers the easy-to-use modeling of sub-structures by nearly any circle and elliptic geometry using shell elements , fully integrated in the ROHR2 framework. This enables to carry out detailed analysis of critical segments inside the framework of the entire model. The shell element sub-structure analysis is carried out using FE-method.

The mesh generator of ROHR2fesu automatically integrates intersections of branches, trunions, and nozzles with and without reinforcement. ROHR2fesu allows controlling the mesh resolution in a simple way. ROHR2fesu has been verified extensively by comparison against reference solutions of standard problems.

ROHR2fesu offers:

- Complete integration of the FE structure(s) into the connecting frame work
- easy-to-use parameter controlled model generation and meshing
- short calculation time
- automatic stress analysis and documentation
- stress analyses following EN 13445, Appendix C, ASME Section VIII, Div. 2, Part 5 and AD S4





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2 Task

The task of ROHR2fesu is the modeling and calculation of shell-sub-structures for the detailed analysis of stiffness and stresses in concentrated segments of the piping structure.

The determination of the substructure in the framework is made on the basis of a stiffness matrix.

The results of a ROHR2fesu calculation are a stiffness matrix and loads at nodes from element loads and extra loads (e.g. loads concentrated on the sub structure) at connection points.

The load cases and load case combinations of the ROHR2 framework model used to determine the element stresses within the shell structure.

The main focus of the application of ROHR2fesu is problems in piping and vessel models where stiffness and/or stress analysis needs to be performed like for:

- Intersections of piping elements generally
- Special components for which internal pressure design stress codes are available but no calculation norms for external forces and moments
- Components where the standards of k- and i-factors are unsatisfactory
- Special components without k- and i-factors defined in the stress codes
- Analysis of local stress utilization
- Optimization of details in pipe and vessel constructions
- Nozzle and cams at vessel with or without reinforcement
- Big diameter tubes with miter bends
- Calculations with to measured pipe segments (as-built), e.g. bends
- Damage analysis at corroded or eroded pipes
- Detail analysis of bend deformation due to internal pressure or bending in oval bends

Of course the standard pipe components (e.g. acc. to EN 13480) can be modeled and calculated in ROHR2fesu.

Stress analyses following EN 13445, Appendix C, ASME Section VIII, Div. 2, Part 5 and AD S4 can be carried out.



ROHR2fesu Feature list Page 3

3 Features

Integration into ROHR2

- Full integration of the shell model as substructure into the framework of the entire piping system
- The stiffness of the shell model is considered in the framework by its stiffness matrix
- Consideration of the loads at the connection to the framework, which result from the substructure
- Easy-to-use modeling of the shell model by combinations of simple basic elements (superelements)
- The coarse model is generated automatically based on the framework
- Automatic generation of connecting elements (interface elements) at the coupling nodes between pipe element based framework and shell element based sub-structures

Superelements/Components

The structure is made of superelements. The super-elements (SE) are combined in groups in ROHR2fesu:

 SE-components pipe
 SE-component
 SE-component
 SE- components head
 SE- components head
 SE- components point
 SE- components point
 SE- components point
 Cone: centric, eccentric, elliptical Bend, circular bend, miter bend, measured bend, creased bend rectangular duct
 Spherical slice toroidal slice - concave, convex elliptic slice
 SE- components point
 Transition element

Superelements/Jackets

- The superelements are defined by a system center line using the start and end node and dimensions at the end node or by cross section areas inside the superelement
- Easy-to use extension and modification of the model by inserting conical or elliptical transitions
- Variable wall thickness across the circumference and elliptical cross sections can be modeled
- Superelements in sequential order are combined in a "jacket"

Intersections

- Intersections can be placed at all superelements except at the connection to the framework
- Fillets at transitions are considered
- Intersections for the modeling of nozzles and trunions with or without reinforcing and internal projection, gusset, rectangular lugs
- Modeling of inserted (block flange) and welded reinforcing pads







Meshing

- Simple meshing of the shell model by defining the axial and circumferential subdivision
- Optimization of model size and calculation time by progressive or regressive division in axial direction
- Individual pre-definition of the mesh of system parts in the intersection segments
- The mesh division can be modified easily

Loads

- Automatic conversion of loads of load cases and load case combination from the framework at the connections between shell model and framework model
- Assignment of operation data (pressure, temperature, medium density) at each load case in the framework analogue to the ROHR2 framework
- Consideration of wind, snow- and ice loads of each load case in the framework
- Consideration of various additional masses, forces and area loads on the sub-structure of each load case in the ROHR2 framework
- Consideration of the axial force from internal pressure at the transition nodes
- ROHR2fesu offers an easy-to-use way to check allowable stresses, e.g. at nozzles

Stress codes

- Stress analysis acc. to EN 13445-3, appendix C due to the method of stress categories
- Stress analysis acc. to ASME Section VIII, Div. 2, Part 5
- Stress analysis acc. to AD S4
- A local area acc. to EN 13445 can be defined easily and the membrane stresses can be regarded as locally which results in a definition as PI

Optimization

- · Simply modification of the system in pipe segments, e.g. fillets, transitions
- Substructures can be optimized independent from each other
- Modifications at a sub-structure does not require the calculation of other sub-structures

Documentation

- Colored representation of element parameters like wall thickness or material
- Graphic representation of utilization and calculated stresses
- Graphic representation of deformations
- Automatic report generation, to be modified by the user







3.1 Integration into ROHR2

ROHR2fesu is fully integrated into the ROHR2win user interface.

Select the segment, to be analyzed detailed, in the framework. From framework details (geometry, dimensions, component type like bend or head) a coarse model of the sub-structure is generated from the selected segment. This model can be completed in ROHR2fesu by details which are missing in the framework. The sub-structure is shown in the containing piping framework using the system lines or as simple shell model. By a double-click on the sub-structure in the framework, ROHR2fesu is launched to change the model or for analysis or documentation of the sub-structure.

The assignment of operation data (pressure, temperature, medium density) at each load case in the framework is done analogue to the ROHR2win framework

ROHR2 calculation of the connecting framework

The stiffness of sub-structure is considered in the framework by a stiffness matrix resulting from the FE-analysis.

ROHR2fesu calculation of the substructure

Loads at the connection points in the framework are automatically taken over into the calculation of the sub-structure.

Loads from the sub-structure are taken over in the framework analysis.









4 Available library of Superelements

4.1 Overview Superelements

The FE structures can be created by nearly any combination and intersection of basic elements (superelements). These superelements are available:

Cone, centric, eccentric, or elliptical / Cylinder (cone special shape)

spenies cone						-
Name S3	Jacket J	2	P1 P3	P2	P5	
Difference coordina	tes [mm]					
DX= 0	DY= 0	DZ= -1	730	Length	1730	
Туре	-+					
Centric (KOZE)		-			_	5 I
eccentric (KOEX) ²	P1			\sim	00
elliptic (ELKO)	· ·	+		-		F2
local						
coordinate		1			_	
(spension)						
Material	ST370 II	-	Materials			
marchar	0.01.0_0	- 11				
Dimensions Imm]						
Dimensions [mm]	Insert outer diam	eter	Insert	mean radiu	JS	
Dimensions [mm] Point	Insert outer diam Outer diameter	eter	 Insert Mean radius 	mean radiu	us Wall th	ickness
Dimensions [mm] Point P1: P3	Insert outer diam Outer diameter Da 1= 508	eter R1=	 Insert Mean radius 250.85 	mean radiu S1=	us Wall th 6.3	ickness
Point Paint Point P2: P5	Insert outer diam Outer diameter Da 1= 508 Da 2= 508	R1=	 Insert Mean radius 250.85 250.85 	: mean radiu S1= S2=	us Wall th 6.3 6.3	ickness
Dimensions [mm] Point 0 P1: P3 1 P2: P5 1 Corre	Insert outer diam Outer diameter Da 1= 508 Da 2= 508 Da 2= 1	eter R1= R2=	 Insert Mean radius 250.85 250.85 Minus mill 1 	mean radiu S1= S2= tolerance	Wall th 6.3 6.3 0.35	ickness
Dimensions [mm] Point P1: P3 P2: P5 Corror Cross section definit	Insert outer diam Outer diameter Da 1= 508 Da 2= 508 Da 2= 1 Da 1= 508	neter R1= R2=	 Insert Mean radius 250.85 250.85 Minus mill f 	mean radiu S1= S2= tolerance	Wall th 6.3 6.3 0.35	ickness
Dimensions [mm] Point (P1: P3 1 P2: P5 1 Corre Cross section definit Plane Syp	Insert outer diam Duter diameter Da1= 508 Da2= 508 Da2= 508 Da30 1 tion for elliptic co Szp Sym	eter R1= R2= nes Szm	 Insert Mean radius 250.85 250.85 Minus mill f Ry 	mean radiu S1= S2= tolerance Rz	us Wall th 6.3 6.3 0.35	New
Dimensions [mm] Point P1: P3 P2: P5 Correc Cross section definit Plane Syp	Insert outer diam Duter diameter Da 1= 508 Da 2= 508 Da 3= 508 Da 5= 508 Da	nes Szm	 Insert Mean radius 250.85 250.85 Minus mill f Ry 	smean radiu S1= S2= tolerance Rz	us Wall th 6.3 0.35	New Edit
Dimensions [mm] Point (P1: P3 1 P2: P5 1 Corre Cross section definit Plane Syp	Insert outer diam Duter diameter Da1= 508 Da2= 508 Da2= 508 Usion 1 Lion for elliptic co Szp Sym	nes	 Insert Mean radius 250.85 250.85 Minus mill f Ry 	s mean radiu S1= S2= tolerance Rz	J8 Wall th 6.3 6.3 0.35	New Edit
Dimensions [mm] Point (P1: P3 1 P2: P5 1 Corre Cross section definit Plane Syp	Insert outer diam Duter diameter Da1= 508 Da2= 508 1 tion for elliptic co Szp Sym	nes	Insert Mean radius 250.85 250.85 Minus mil 1 Ry	mean radiu S1= S2= tolerance Rz	US Wall th 6.3 6.3 0.35	New Edit Delete
Dimensions [mm] Point P1: P3 P2: P5 I Corre Cross section definit Plane Syp Distribution	Insert outer diameter Duter diameter Da1= 508 Da2= 508 ison 1 ison for elliptic co Szp Sym	nes Szm	Insert Mean radius 250.85 250.85 Minus mil 1 Ry	smean radiu S1= S2= tolerance Rz	Wall th 6.3 6.3 0.35	New Edit Delete
Dimensions [mm] Point (P1: P3 1 P2: P5 1 Correc Cross section definit Plane Syp Distribution in axial direction 1	Insert outer diameter Dater diameter Da 1= 508 Da 2= 508 Da 3= 508 Da 5= 508	eter R1= R2= Szm	Insert Mean radius 250.85 250.85 Minus mill 1 Ry	Rz rection 60	Us Wall the 6.3 6.3 0.35	New Edit Delete
Dimensions [mm] Point (P1: P3 1 P2: P5 1 Correc Cross section definit Plane Syp Distribution in axial direction 1 Progression	Insert outer diameter Da1= 508 Da2= 508 sion 1 tion for elliptic co Szp Sym 5 elemen	eter R1= R2= Szm	(@) Inset (%)	Rz rection 60	US Wall the 6.3 6.3 0.35	New Edit Delete

The definition of the cone can include the parameters:

- Туре
- Material
- Outer diameter / radius at start/ end node
- Wall thickness
- Minus-mill tolerance
- Element division in axial and circumferential direction

The superelement cone also can be used for the modeling of a nearly flat plate.

Pipe bend as Ideal sound bend, miter bend or measured bend

The definition of the cone can include the parameters:

- Type
- Material
- Outer diameter / radius
- Wall thickness
- Minus-mill tolerance
- Element division in axial and circumferential direction

At measured bends additionally the radii and wall thickness' can be defined for each cross section around the circumference.

roperties	bend					2
Name	e S6	Jacket J1	P	1 P8	P2 P6	
Fangent	intersection PT	P7	Radius	1016.21	mm	
Type Ideal (RU Miter (SEC (SEC (IST)	round bend BO) bend BB) sured bend B) sed bend	a l	P1 *	NR /	>	
(RU)	30)			/	P2	
Aaterial	ST37.0_U	•	Materials	No	of segments	1
D Солов	a1= 1016 sion 1	R1= 50	0.9 linus mill tolera	S1= 14,2 ance 1.775		
Cross s	ection definition	for measured ben	Cam D			
1	14.20 14 14.20 14	20 14.20 .20 14.20	14.20 5	500.9 500 500.9 500).9).9	New Edit
Creased	d bend No. of creas	es 0	Height of crea	ases 0	mm	Delete
Distribu	tion					
in axial	direction 10	elements	in circumfe	erential directi	on 60	elements
Prog	ression	(the all	e distribution in elements of th	n circumferen ne jacket)	ntial direction is	s valid for





Rectangular duct

The definition of the rectangular duct can include the parameters:

- type
- material
- length/width, radius of the corner
- wall thickness
- minus-mill tolerance
- element division in axial direction and length/width



Spherical slice or ellipsoid slice

Name S3		Jacket J1		P1 P4	P2	P43	
Difference coord	linates (m	m]					
DX= 0.192716	DY=	-1110.9994	DZ= 0.	187555	Length	1110.999	948
A	-		а /		1	7	
Aaterial ST37.0	R1		aterials	Sphere ra	adius (RKug	i) -1.0000)0(mm
Material ST37.0 Dimensions [mm]	NI U I I I Insert	M	aterials	Sphere ra	adius (RKug t mean radiu	i) -1.0000 Js Wall thick)O(mm
Aaterial ST37.0 Dimensions [mm] Point P1: P4	R1	M outer diameter ter diameter 1016	aterials R1=	Sphere ra Inser Mean radius 500.9	adius (RKug t mean radiu s S1=) -1.0000 Js Wall thick 14.2)O(mm kness
Aaterial ST37.0 Dimensions [mm] Point P1: P4 P2: P43	LU I Insert Ou Da1= Da2=	M outer diameter ter diameter 1016 1016	R1= R2=	Sphere ra Inser Mean radius 500.9 500.9	adius (RKug t mean radiu S1= S2=) -1.0000 Wall thick 14.2 14.2	000 mm kness
Aterial ST37.0 Dimensions [mm] Point P1: P4 P2: P43 C	_U I Da1= Da2= orrosion	M outer diameter ter diameter 1016 1016 1	aterials R1= R2=	Sphere ra Inser Mean radius 500.9 500.9 Minus mill t	adius (RKug t mean radiu S1= S2= olerance	i) -1.0000 Js Wall thick 14.2 14.2 1.775	000 mm kness
Aaterial ST37.0 Dimensions from Point P1: P4 P2: P43 C Distribution in axial direction Progression	_U Da1= Da2= orrosion	M outer diameter ter diameter 1016 1016 1 elements th all	R1= R2= in circume distribution	Sphere ra (a) Inser Mean radius 500.9 500.9 Minus mill t mferential dir on in circum of the jacket	t mean radiu S1= S2= olerance ection 60	i) -1.0000 Wall thick 14.2 14.2 1.775 ection is v	000 mm kness ements ralid for

The definition of the spherical slice can include the parameters:

- Material
- Outer diameter / radius at start/ end node
- Wall thickness
- Corrosion allowance
- Minus-mill tolerance
- Element division in axial and circumferential direction

Alternatively an ellipsoidal slice can be defined in ROHR2fesu.



Using these superelements nearly all components used in practice can be modeled. For examples, please see 5.



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Torus, convex or concave



The definition of the torus can include the parameters:

- Material
- Type convex / concave
- Outer diameter / radius at start/ end node
- Wall thickness
- Corrosion allowance
- Minus-mill tolerance
- Element division in axial and circumferential direction



Torus concave as shown in the dialog window



Without fillet



with fillet

Elliptic slice

The definition of the elliptic slice can include the parameters:

- Material
- Type convex / concave
- Outer diameter / radius at start/ end node
- Wall thickness
- Corrosion allowance
- Minus-mill tolerance
- Element division in axial and circumferential direction







4.2 Connections to the framework

Transition elements are inserted the connection to the framework (transition elements). A transition element is the connection between a shell and a beam. The transition element consists of a short hub (centered pipe stump) with rigid spokes, leading to the shell points at the circumference. According to the Bernoulli Hypothesis of linear statics it guarantees the flatness of the cross section at the limit of the shell model.

In special cases the degrees of freedom of the couplings at the shell can be modified.

4.3 Intersections

The program allows inserting intersections for the modeling of nozzles and trunions with or without reinforcement and internal projection. The model of the reinforcing pad may be entered as single shell or double shell with material selectable for the reinforcing pad.

The meshing is done for partial regions inside the intersection area.

Inserted values are explained by expandable detail drawings.

The intersection includes the parameters

- Type: Nozzle or trunion
- Fillet radius on the surface
- Element distribution
- Internal projection
- Reinforcing pad with details:
 - single shell/double shell
 - width
 - thickness
 - material



Reinforcing pad ↓ with reinforcing pad Type of model: ● single-s	hell 🔿 dou	ble-shell
Width of the reinforcing pad (AKrag)	30	mm
Add, thickness of the jacket wall in the regoin of	5	mm
No. of elements on the reinforcing pad (nFEK)	8	
Material 5T37.0		

Examples: fillet or reinforcing slice



Intersection with fillet



Intersection with reinforcing slice





4.4 Loads

The connecting framework influences the sub-structure by its loads. The loads are transmitted into the sub-structure at transition nodes. This does not require special load inputs in the FE model. Loads from load cases and load case combinations in the framework are taken over into the FE model.

Loads, occurring in the sub-structure are assigned in the framework model, too. Among them:

- Operation data (pressure, temperature, medium density)
- Wind loads (determined automatically or manually entered)
- Snow loads
- Ice loads
- additional masses
- any additional forces
- any loads on areas

The insulation parameters of automatic determined loads form snow, ice and wind are taken from the following segments in the framework. They are considered approximately when calculating the loads in the sub-structure.

Loads at the entire system (framework model) occurring at transition nodes, which are resulting from the sub-structure analysis, are considered in the framework model.

4.5 Model generation restrictions

Even though the generation of the shell sub-structure from the piping system is very generic a few limitation apply in order to allow a smooth integrated meshing and calculation: but the intersection of super elements causes a few limitations.

- Only one pressure, one temperature and one medium density can be assigned to each substructure and load case
- Assignment of materials can be done only for each superelement
- Opposite nozzles may not though themselves
- Only one superelement can be active in an intersection
- The intersection always needs to go through the entire cross-section of the nozzle
- An intersection at connection points of several jackets (e.g. branching of pipe jackets a skirt support) or transition element are not allowed
- At one end of the superelement an intersection is allowed. At the other end a cross section vertical to the axis is required. If necessary the superelement can be divided by an intermediate node.
- Intersections cannot be intersected again



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4.6 Stress analysis

A stress analysis is carried out for the sub-structure following EN 13445, Appendix C, ASME Section VIII, Div. 2, Part 5 and AD S4.

. The generation of load case superpositions and required analyses is done in ROHR2win using the defined load cases or it can be entered manually. Load cases and stress utilization for each analysis at the shell elements are shown in the graphic.



In the analysis of the local membrane stresses (PI) only the segment is shown, where the calculated stress

is > 1.0 x f which means that they must be characterized as local. An easy-to –handle measuring instrument can be used to verify if the selected part is really a local area according to EN 13445. In the intersection area the measured width in meridional direction is automatically compared to the maximum value ls+ln of EN13445.

Max Ausn. = Max Stress Utilization

4.7 Results representation

At each analysis the model can be shown as completely deformed shape or the deformations are shown in an additional wire frame model.

10.9 mm < 25.8 mm

Max. Ausn.: 91.7 %



Connection loads and movements at transition elements can be displayed.







4.8 Results documentation

ROHR2fesu automatically generates a report in rtf format after the calculation showing essential results. The report generation is carried out using a report template. Predefined templates are available in German and English. They can be modified by the user.

The reports are updated automatically after re-calculation.

Sample ROHR2fesu - report template





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5 Examples

The ROHR2fesu examples listed here are shown in a reduced size. For bigger drawings and additional comments please go to ROHR2fesu at www.rohr2.com.

Simple sloping branch





A simple (sloping) branch is created by two superelements of the type *Centric Cone*. For the intersection it must be defined properties like rounding radius, projection or reinforcement.

Norm-Tee with conical transitions



The cylindrical bases of the norm tee are created by superelements type *Cylinder*. The conical transitions in the center of the tee are superelements of the *Centric cone* with different dimensions at the beginning and at the end. The intersection requires the input of a fillet.

Spherical fitting





The cylindrical bases as well as the conical transitions are made by superelements of the type *Centric Cone*. The sphere is created by the superelement *Spherical Slice* (in the special form complete sphere).





Support at bend





The support and the cylindrical bases are created by the superelement of the type *Centric Cone*. The bend is created by a superelement of the type *bend* (here round bend).

Branch in eccentric reducer





The nozzle and the cylindrical bases are created by a superelement of the type *Centric cone (cylinder)*. The reducer is created by a superelement of the type *Eccentric Cone*.



The cylindrical bases are created by superelements of the type Centric Cone (cylinder). The two "reducers" are made by superelements type *Eccentric Cone*





Complex systems







Rectangular lug and Gusset





6 Program license and system requirements

Program version, network license

ROHR2fesu is an optional available module in the program system ROHR2. It can be part of the ROHR2 single user license and ROHR2 network license. In the ROHR2 network license the number of the users of an optional module can be similar or lower than the number of ROHR2 network seats. For system requirements and program features see ROHR2 Specification. Running ROHR2fesu requires the installation of **ROHR2**.

Scope of delivery and Copy protection

The programs' scope of delivery contains

- the program data (by download or ROHR2 CD)
- the program documentation in html and/or pdf format)
- unlocking the module on the ROHR2 license key (USB, dongle).

The software does not run without the license key. In case of updates/upgrades the license key will be replaced or updated.

Documentation /User manual

The functions of ROHR2fun are part of the ROHR2win manual and explained in the ROHR2fesu manual (pdf document).

Maintenance and user support

Advice about installation and application is done by the ROHR2 user support (hotline). The hotline is part of the included service after purchase, during time limited licensing (rent) and as a part of a maintenance agreement.

Interfaces and additional programs are integrated into ROHR2. Maintenance of additional programs and interfaces is mandatory in this case.

7 Software Development, Sales and Support

SIGMA, established in 1989 in Dortmund, Germany has emerged as a partner of choice for leading international companies with its software and the wide variety of engineering services. SIGMA is known as one of the leading engineering specialists in the Pipe Stress Business in Europe, offering field tested products, strongly adapted to the user's needs.

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